Water Supply and Distribution Management

## Question 1 (34 marks)

The following pipe network and the associated pipe and node data are given in Figure Q1 and Tables Q1a and Q1b. The fixed head reservoir (water elevation equal to 45 m ) is located at node 1 .


Figure Q1. Network Layout
Table Q1a. Network Pipe Data

| Pipe | Length <br> $(\mathrm{m})$ | Diameter <br> $(\mathrm{mm})$ | Absolute <br> Roughness <br> $(\mathrm{mm})$ |
| :---: | :---: | :---: | :---: |
| 1 | 500 | 250 | 0.1 |
| 2 | 600 | 200 | 0.1 |
| 3 | 500 | 100 | 0.1 |
| 4 | 1000 | 150 | 0.1 |

Table Q1b. Network Node Data

| Node | Elevation <br> $(\mathrm{m})$ | Demand <br> $(\mathrm{l} / \mathrm{s})$ |
| :---: | :---: | :---: |
| 2 | 10 | 10 |
| 3 | 20 | 20 |
| 4 | 18 | 15 |

(a) Calculate the unknown pipe flows and nodal pressure heads in the above system by performing the first two iterations of the Hardy-Cross method.

$$
\text { (i) Iteration } 1
$$

(ii) Iteration 2
(b) Assuming the target (head loss) accuracy of $\varepsilon H=0.01 \mathrm{~m}$, calculate the pipe flows. (4 marks)
(c) If the minimum pressure requirement at demand nodes is 25 m , comment on the system's ability to supply the specified demand with adequate pressure.

## Question 2 (33 marks)

During a 24 -hour period the river flows Qinf, shown in Table Q2a, were recorded immediately upstream of a water supply reservoir shown in Figure Q2.

Table Q2a. Reservoir Inflows

| Time <br> period | Qinf <br> $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ |
| :---: | :---: |
| 0 a.m.-4 a.m. | 6.50 |
| 4 a.m. -8 a.m. | 5.00 |
| 8 a.m. -12 p.m. | 9.00 |
| 12 p.m. -4 p.m. | 7.00 |
| 4 p.m. -8 p.m. | 5.00 |
| 8 p.m. - 0 a.m. | 4.50 |



Figure Q2. Reservoir schematic

During the same period, the storage levels, shown in Table Q2b, were recorded for the reservoir.

Table Q2b. Reservoir Storage

| Time | Storage <br> $\left(\mathrm{m}^{3}\right)$ |
| :---: | :---: |
| 0 a.m. | 300,000 |
| 4 a.m. | 350,400 |
| 8 a.m. | 328,800 |
| 12 p.m. | 350,400 |
| 4 p.m. | 357,600 |
| 8 p.m. | 292,800 |
| 0 a.m. | 300,000 |

(a) Determine the water supply hydrograph, $\operatorname{Qws}(t)$ taken directly from the reservoir if the required environmental release is fixed at Qenv $=0.5 \mathrm{~m}^{3} / \mathrm{s}$ and assuming that there were no spills from the reservoir during this 24 -hour period.
(13 marks)
(b) Comment on the reservoir's ability to supply the specified demands on a longterm basis.
(10 marks)
(c) Determine the uniform demand that can be supplied from the reservoir assuming that the inflow sequence will be repeated in the future.
(10 marks)

## Question 3(33 marks)

Water is pumped from reservoir A to reservoir B through a 250 mm diameter pipeline $A B$, as shown in Figure Q3.


Figure Q3. Pump System

The pipeline's Hazen-William roughness coefficient is equal to 110. The pump characteristics are given in Table Q3.

Table Q3. Pump Characteristics

| Flow (litres/s) | 0 | 20 | 40 | 60 | 80 | 100 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Head $(\mathrm{m})$ | 110 | 108 | 105 | 95 | 75 | 40 |
| Efficiency | 0 | 0.62 | 0.80 | 0.85 | 0.80 | 0.60 |

(a) Determine the flow rate through the system and the pump's head and efficiency at this flow rate.
(25 marks)
(b) A second pump of identical characteristics is installed in parallel to the original one. Determine the flow rate through the new system and the head and efficiency of the pumps in parallel assuming that any additional head losses created by pump parallelisation are negligible.
(8 marks)

## ECMM133 Formula Sheet

## Pipe Flow Formulae:

Darcy-Weisbach:

$$
h_{f}=\lambda L / D v^{2} / 2 g
$$

Laminar Flow: $\lambda=64 / R_{e}$
Turbulent Flow: $1 / \sqrt{\lambda}=-2 \log _{10}\left[k /(3.7 D)+2.51 /\left(R_{e} \sqrt{\lambda}\right)\right] \quad$ (Colebrook-White)
$1 / \sqrt{\lambda}=-2 \log _{10}\left[k /(3.7 D)+5.74 /\left(R_{e}{ }^{0.9}\right)\right] \quad$ (Swamee-Jain)
Hazen-Williams:

$$
v=0.355 C D^{0.63} S_{f}^{0.54} \quad \text { where } S_{f}=h_{f} / L
$$

General Formulation:

$$
h_{f}=R \cdot Q \cdot / Q /^{n-1}
$$

Darcy-Weisbach: $R=0.8106 \lambda L /\left(g D^{5}\right) \quad$ and $n=2.0$
Hazen-Williams: $R=10.648 L /\left(C^{1.852} D^{4.871}\right)$ and $n=1.852$

## Valve Flow:

$$
Q=C_{d} A \sqrt{2 g \Delta H_{v}}
$$

## Hydraulic Solvers:

Hardy-Cross Method:

$$
\Delta Q_{i}^{(k)}=\frac{-\sum_{i} h_{f, i}^{(k)}}{n \sum_{i} \frac{h_{f, i}^{(k)}}{Q_{i}^{(k)}}} \quad Q_{i}^{(k+1)}=Q_{i}^{(k)}+\sum_{l \supset i} \Delta Q_{l i}^{(k)}
$$

Linear Theory Method:

$$
H_{i}^{(k+1)}=\frac{\sum_{j}^{N_{i}} \frac{H_{j}^{(k)}}{U_{i j}^{(k)}}-Q_{d, i}}{\sum_{j}^{N_{i}} \frac{1}{U_{i j}^{(k)}}} \quad Q_{i j}^{(k+1)}=\frac{H_{i}^{(k+1)}-H_{j}^{(k+1)}}{U_{i j}^{(k)}} \quad U_{i j}^{(k)}=R_{i j}\left|Q_{i j}^{(k)}\right|^{n-1}
$$

## Water Properties:

Density $=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Kinematic Viscosity $=1.14 \times 10^{-6} \mathrm{~m}^{2} / \mathrm{s}$
Bulk Modulus (Coefficient of Compressibility) $=2.15 \times 10^{9} \mathrm{~N} / \mathrm{m}^{2}$

